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3	High Pressure Effects on the Iron-Iron Oxide and Nickel-
4	Nickel Oxide Oxygen Fugacity Buffers
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22 Abstract

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24 The chemical potential of oxygen in natural and experimental samples is 25 commonly reported relative to a specific oxygen fugacity (fO_2) buffer. These buffers are 26 precisely known at 1 bar, but under high pressures corresponding to the conditions of the deep Earth, oxygen fugacity buffers are poorly calibrated. Reference (1 bar) fO₂ buffers 27 28 can be integrated to high pressure conditions by integrating the difference in volume 29 between the solid phases, provided that their equations of state are known. In this work, 30 the equations of state and volume difference between the metal-oxide pairs Fe-FeO and 31 Ni-NiO were measured using synchrotron x-ray diffraction in a multi-anvil press and 32 laser heated diamond anvil cells. The results were used to construct high pressure fO_2 33 buffer curves for these systems. The difference between the Fe-FeO and Ni-NiO is 34 observed to decrease significantly, by several log units, over 80 GPa. The results can be 35 used to improve interpretation of high pressure experiments, specifically Fe-Ni exchange 36 between metallic and oxide phases.

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38 *Keywords*: oxygen fugacity; high pressure; equations of state.

39 1. Introduction

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The chemical potential of oxygen is frequently as important as temperature or pressure in controlling the chemical and physical behavior of minerals. Variations in the oxygen potential can cause insulator-metal transformations, for example, or drive large changes in diffusion rates and rheological properties through its control over vacancy populations. Perhaps most important to geochemical consideration, the chemical potential of oxygen can have great effect on elemental partitioning between coexisting phases, particularly when the chemical exchange involves a redox reaction.

48 In high-pressure, high-temperature geochemistry experiments, the oxygen 49 fugacity (fO_2) is frequently set by, or determined in relation to, a metal-oxide fO_2 buffer 50 (e.g., Fe-FeO, Ni-NiO, Re-ReO₂) (Dobson and Brodholt, 1999; Rubie, 1999). To compare 51 the experimental results to one another, it is important to know how these buffers change 52 with pressure; otherwise the redox dependence determined by comparison of differently-53 buffered experiments will be systematically in error. For example, high pressure metal-54 silicate reactions have been extensively studied using multi-anvil apparatus (e.g., 55 Thibault and Walter, 1995; Li and Agee, 1996; 2001; Righter et al., 1997; Ohtani et al., 56 1997; Walter et al., 2000; Righter, 2003; Wade and Wood, 2005; Corgne et al., 2008; 57 Kegler et al., 2008), and the various systems used as reference buffers in those 58 experiments are imperfectly calibrated against one another at high pressures. Moreover, 59 recent improvements in sample preparation techniques and microanalytical tools have 60 turned the diamond anvil cell into a petrological tool, used to study phase relations and 61 elemental partitioning between phases in recovered high-P,T samples (e.g., Irifune et al., 62 2005; Takafuji et al., 2005; Auzende et al., 2008; Riccoleau et al., 2008; Sinmyo et al., 2008). As diamond cell technology continues to advance, with improved methods for 63 64 microanalysis of chemical distributions in the high-pressure samples, the chemical 65 activity of oxygen will become an increasingly important factor for interpretation of the

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66	experimental r	results, comparable to the important role fO_2 control plays in lower pressure
67	petrological st	udies. Likewise, increasingly sophisticated computer simulations of
68	chemical react	ions at high pressure can be expected to advance into high-pressure
69	petrological st	udies. The activity of oxygen in these simulations can be varied by
70	adjusting the n	number of oxygen atoms in the system (e.g., Zhang and Oganov, 2006).
71	Placing these 1	new experimental and computational results in a thermodynamic
72	framework inc	luding oxygen fugacity will greatly facilitate the understanding of the
73	results, and als	so permit separate experiments to be more usefully compared to one
74	another.	
75	Oxyge	n fugacity (fO_2) is a proxy for the chemical activity of oxygen (a_{02}) in a
76	system. For the	e general metal-oxide equilibrium reaction
77	(1)	$M + x/_2 O_2 = MO_x$
78	the fO_2 is relate	ed to the Gibbs energies (G) by
79	(2)	$x_2 \operatorname{RT} \ln f \operatorname{O}_2 = G(\operatorname{MO}_x) - G(\operatorname{M}) = \Delta G$
80	where ΔG is the	he difference in Gibbs energy between the oxide (MO _x) and metal (M)
81	phases. The pr	ressure effect on the fO_2 buffer is thus related to the change in ΔG with
82	pressure. Alon	g each isotherm, $\partial G/\partial P _{T} = V$, so the effect of pressure on fO_2 depends on

83 the volume difference (ΔV) between oxide and metal:

84 (3)
$$\partial (\ln f O_2) / \partial P|_{\mathrm{T}} = (2/\mathrm{x} \mathrm{R} T) \Delta V$$

85 One can construct high pressure fO_2 buffer curves by integrating equation (3)

86 isothermally to a specified pressure, using appropriate equation of state data for each

87 phase buffering the oxygen activity (metal and oxide, in the example here). However,

some of the relevant equations of state are poorly known even for commonly used buffermaterials.

90 In this study we present high pressure, high temperature oxygen fugacity curves

91 for the Fe-FeO and Ni-NiO reactions. These buffers were chosen for their great

- 92 importance to deep Earth geochemical studies. The Fe-FeO reaction dominates the redox
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93 conditions of the deep Earth because of the association of the metallic core with a mantle 94 containing significant amounts of oxidized iron. Consequently, many high pressure 95 geochemical experiments are performed under conditions close to this buffer. Likewise, 96 the Ni-NiO buffer is widely used to produce more oxidizing conditions in geochemical or 97 petrological experiments. Of particular importance are studies of metal-silicate 98 partitioning, that are carried out to understand the observed budget of moderately and 99 highly siderophile elements in the mantle. Nickel is a key trace element in these studies, 100 because its well-constrained mantle abundance (McDonough and Sun, 1995) is thought 101 to be a consequence of metal-silicate equilibration during core-mantle segregation in the 102 early Earth (Li and Agee, 1996; Ohtani et al., 1997).

103 To determine these high pressure buffer curves, we propagate the well-established 104 1 bar buffers to high pressure using equation (3). The high-P,T values of ΔV that we use 105 are determined experimentally by in situ X-ray diffraction measurements of the metal-106 oxide pairs coexisting under identical high-P,T conditions. Comparing V between two 107 independently measured equations of state compounds the errors associated with them. 108 Therefore, we measured coexisting metal-oxide buffer pairs simultaneously, which 109 minimizes systematic biases that might appear between separate studies and improves the 110 precision of the ΔV data used to determine the high pressure fO_2 buffers. A wide range of 111 P,T conditions, exceeding 65 GPa and 2400 K, was covered by the use of two different 112 high-pressure technologies, the multi-anvil press (MAP) and the laser-heated diamond 113 anvil cell (DAC).

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117 **2. Experimental**

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- 119 2.1. Multi-anvil press
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121 The multi-anvil press (MAP) samples were prepared in the Johnson Space Center 122 high-pressure laboratory. The sample materials were mixtures of 1:1 by weight of Ni:NiO 123 or Fe:Fe_{1-x}O, all obtained from Alfa Aesar. These were then mixed with 50% NaCl by 124 weight, which acted as an internal pressure standard and also helped to distribute the 125 sample material, inhibiting excessive grain growth that would deleteriously affect the x-126 ray diffraction measurements. Each high-P,T run included either Ni:NiO or Fe:Fe_{1-x}O, not 127 both. The sample mixtures were loaded into a boron nitride capsule and set into either a 14/8 or 10/5 octahedral MAP assembly. These octahedral assemblies were developed by 128 129 the COMPRES multi-anvil assembly initiative, and were designed specifically for use in 130 synchrotron-based multi-anvil experiments (Leinenweber et al., 2006). The 14/8 G2 in 131 situ assembly is a graphite box furnace with a forsterite insulating sleeve. The heater and 132 sleeve were x-ray transparent, easily permitting x-ray diffraction measurements, but 133 heating was limited to < 1000 °C, < 13 GPa to avoid graphite-to-diamond conversion. 134 The 10/5 in situ assembly expanded the pressure range achievable, and temperature was 135 limited by melting of the NaCl. X-ray transmission through the Re foil heaters was 136 allowed by fabricated small slits aligned with Al₂O₃ windows in the LaCrO₃ insulating 137 sleeve. This allowed x-ray transmission through the sample chamber, but introduced 138 Al₂O₃ diffraction peaks in the measured spectrum.

The octahedral assemblies were loaded into the 1000-ton multi-anvil press at
beamline 13-ID-D of the GSECARS sector of the Advanced Photon Source (Uchida et
al., 2002). The samples were oven dried before loading them into the press. They were
then pressurized for in situ, high-*P*,*T* X-ray diffraction using synchrotron radiation. The
x-ray source was a white beam, collimated to approximately 100 μm x 100 μm using two

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pairs of WC slits. Diffracted X-rays were measured using a Ge solid state energy
dispersive detector at a fixed angle of 6.1°. The detector had 4000 channels, and the
exposure times were typically 5 minutes.

In most experiments, the sample was pressurized to its maximum pressure (~12 GPa in these experiments) before any equation of state data were collected. Then the sample was heated to the maximum target temperature, which caused some reduction of pressure. Pressure-volume-temperature (P-V-T) diffraction data were collected on cooling cycles, when non-hydrostatic stresses had been relaxed. After each cooling cycle, the press load was reduced, the sample was heated, and data collection resumed on the next cooling cycle. Data were collected in temperature intervals of 200 °C.

154 The detector angle was calibrated using the zero pressure lattice spacing of NaCl (a = 5.6402 Å, JCPDS card #05-0628), measured from each sample before initial 155 156 compression. The recorded x-ray diffraction patterns were analyzed using PeakFit (Systat 157 Software, Inc.); this involved background subtraction and peak fitting, including 158 deconvolution of overlapping peaks. In addition to the sample materials, the NaCl 159 pressure standard, and the Al₂O₃ windows, both diffraction and x-ray fluorescence from 160 the Re foil heaters were sometimes detected. Lattice parameters were calculated from at 161 least 3 lines for all samples of hexagonal symmetry, and at least 2 lines for isometric 162 samples. Uncertainties on the lattice parameters reflect standard deviations from multiple 163 diffraction peaks. Pressures were determined from the Decker equation of state for the B1 164 phase of NaCl (Decker, 1971).

165 Stoichiometric FeO is only stable at high *P* and *T*; at lower pressures and 166 temperatures non-stoichiometric wüstite is observed, with variable composition, even 167 when coexisting at equilibrium with Fe metal (Stølen and Grønvold, 1996). We used 168 ΔV_{IW} data only from the *P*-*T* range in which stoichiometric FeO coexisted with fcc-Fe 169 according to the model B phase diagram of Stølen and Grønvold (1996); their model B 170 was chosen because the bulk modulus values in that model are consistent with those in

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171 Fei (1996) and Haavik et al. (2000), and also the bulk modulus determined in the present 172 study. Stølen and Grønvold's (1996) result is that FeO coexisting with Fe metal is 173 stoichiometric above 5 GPa at 900 K, with a slope < -120 K/GPa. 174 175 2.2. Laser-heated diamond anvil cell 176 177 The diamond anvil cell (DAC) samples were prepared in the University of 178 Maryland Laboratory for Mineral Physics. The sample materials were mixtures of either 179 Ni-NiO or Fe-Fe_{1-x}O, using similar materials as were used in the MAP experiments, and 180 were finely ground to $\sim 1 \,\mu m$ grain size in an agate mortar. These mixtures were 181 compressed into a thin flake, approximately 3-6 µm in thickness (which may further 182 decrease by tens of percent at high compression), and then loaded into the sample 183 chamber of a symmetric-type DAC, between layers of NaCl insulator. The gaskets were 184 stainless steel or rhenium, 250 µm thick before indentation. Anvils having culet 185 diameters of 250 to 400 µm were used, and holes of 80 to 130 µm were formed in the 186 center of the preindented gaskets using an EDM (Hylozoic Products, Inc.). 187 Synchrotron X-ray diffraction measurements (Figure S1 in the Supplementary 188 Material) were carried out while laser-heating the samples at beamline 13-ID-D of the 189 GSECARS sector of the Advanced Photon Source. Details of the optical system are given 190 by Shen et al. (2005). The X-ray source was a monochromatic beam ($\lambda = 0.3344$ Å) 191 measuring 5 µm x 5 µm, and diffracted x-rays were recorded using a MAR345 CCD area 192 detector. The sample-to-detector distance was calibrated by 1 bar diffraction of CeO₂. 193 Exposure times were typically 5 s. 194 The samples were heated on both sides using a Nd:YLF laser operating in either 195 TEM₀₀ or TEM_{01*} mode. The laser spot sizes were 30-40 µm, much larger than the X-ray 196 beam, and were coaligned with the beam by taking advantage of X-ray induced 197 fluorescence from the NaCl insulator. Laser powers were adjusted to equalize the

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temperature on the two surfaces of the sample, usually to within <50 K. Temperatures
were measured from 5 μm diameter areas in the center of the laser heated spots on both
side of the sample. The spectroradiometric method (Heinz and Jeanloz, 1987) was used,
with the graybody approximation, over the 600-800 nm range of thermal emission. The
precision of fit to the thermal emission spectra was typically better than 1%; as discussed
by Kavner and Panero (2004) and Campbell et al. (2007), the greatest contribution to
uncertainty in the temperature measurements is the presence of thermal gradients,

especially in the axial direction through the thickness of the sample. Based on the thermal modelling of Campbell et al. (2007), we estimate that the average temperature of the sample within the region probed by X-ray diffraction is typically 3% less than the measured surface temperatures, for the experimental parameters used in these measurements. Accordingly, our reported temperatures have been corrected by -3% (0.03 x ($T_{meas} - 295$ K)), and an uncertainty equal in magnitude to this correction has also been applied to our error estimates.

212 The use of X-ray diffraction during the high-P,T experiment permits pressure 213 determination by an internal standard, whose high-P,T equation of state is known. In 214 these experiments we use the NaCl insulator as a pressure standard. The advantages of 215 this are that the equations of state of both the low-pressure (B1) and high pressure (B2) 216 phases of NaCl are well determined under high-P,T conditions (Decker, 1971; Fei et al., 217 2007), and also that the same material is then used in all of the Fe-FeO and Ni-NiO 218 experiments reported here, whether in the MAP or the DAC. A disadvantage of using the 219 insulator as the pressure standard is that the mean temperature of the standard is then not 220 equal to the mean temperature of the sample, because of the temperature gradient across 221 the NaCl layer from the hot sample surface to the cool (approximately 295 K) diamond 222 anvil surface. However, as demonstrated below and in Mao et al. (2007), the uncertainties 223 of this method are only a couple of GPa or less, so the resulting P-V-T measurements are 224 well constrained for our present purpose.

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225 The temperature distribution in the sample and the NaCl insulator during laser 226 heating is schematically illustrated in Figure 1. The distribution within the sample was 227 calculated from the diffusion equation, with a gaussian distribution imposed on the 228 sample surfaces as boundary conditions (Campbell et al., 2007). The temperature 229 gradient across the NaCl layers, in the region probed by the X-ray beam, lies between 230 T_{meas} at the sample surface to T_{anvil} at the anvil surface, and the average temperature over 231 which X-rays are diffracted from the pressure medium, T_{NaCl} , is $(T_{\text{meas}}-T_{\text{anvil}})/2$. Departures 232 from linearity of this gradient may result from several sources, including: non-constant 233 diffusion coefficient of thermal diffusion in NaCl with varying temperature; radiative 234 heat transfer; and radial heat flow from the central axis to the cooler surrounding region. 235 These factors are small, and partly compensating for one another. We assume the 236 midpoint between sample surface and anvil surface temperatures to be the mean 237 temperature of the pressure standard; the sample temperature is measured 238 spectroradiometrically, and the anvil temperature must lie between room temperature 239 (295 K) and T_{meas} : $T_{\text{anvil}} = (T_{\text{meas}} + 295)/2 \pm (T_{\text{meas}} - 295)/2$. Therefore, as illustrated in Figure 240 1, the effective temperature through the NaCl medium can be taken to be 241 (4) $T_{\text{NaCl}} = (3T_{\text{meas}} + 295)/4 \pm (T_{\text{meas}} - 295)/2$

This translates to a typical error in pressure of only 2-6%, because of the high
compressibility of NaCl relative to its thermal expansion. Separate, unpublished, tests of
this method of calibration using a Pt sample (whose equation of state is calibrated against
NaCl by Fei et al., 2007) confirm that Equation (4) yields an appropriate measure of
pressure in the sample geometry of Figure 1.

247 Deviatoric stresses are significant in an unheated diamond anvil cell at room 248 temperature; however, at high temperatures these stresses are minimized by relaxation of 249 the sample and pressure medium (Kavner and Duffy, 2001). Under these high 250 temperature conditions, the assumption of mechanical equilibrium (i.e., constant pressure 251 between the metal, oxide, and pressure standard) is reasonable. However, our results

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- below show that at low temperature, following rapid quench of the laser heated sample,
- residual strains remain in the cell and the assumption of mechanical equilibrium may no
- longer hold, as also observed by Kavner and Duffy (2001).

3. Results

257	Tables S2 and S3 of the Supplementary Material contain the <i>P</i> - <i>V</i> - <i>T</i> data for the
258	Fe-FeO and Ni-NiO experiments respectively. Each table contains: the molar volumes of
259	each phase (metal, oxide, and NaCl pressure standard); the corresponding $\Delta V (= V_{ox} - V_{met})$;
260	the temperatures of the sample and the NaCl (corrected as in Section 2.2); and the
261	pressure determined from the equation of state of NaCl (Decker, 1971; Fei et al., 2007).
262	In Table S2, the structure of the Fe phase (fcc or hcp) is also indicated. Only those
263	phases that were stable under the indicated <i>P</i> , <i>T</i> conditions (Shen et al., 1998) are
264	included; occasionally a metastable phase of Fe was observed, but these molar volumes
265	are not reported. All reported data have FeO in the B1 structure. The high-pressure
266	rhombohedral phase of wüstite (Fei and Mao, 1994) exists only at temperatures lower
267	than those needed for our intended application of constructing high-pressure fO_2 buffers.
268	At high pressures and high temperatures a B8-type phase of $Fe_{1-x}O$ has been reported (Fei
269	and Mao, 1994; Murakami et al., 2004), but this phase was not seen in our results nor in
270	those of Seagle et al. (2008). We speculate that this could be because of the stoichiometry
271	of our FeO phase ($x = 0$). In addition to the data listed in Table S2, our analysis includes
272	the <i>P-V-T</i> data from Seagle et al. (2008), who used virtually identical experimental
273	methods in their DAC study of the Fe-FeO system. The molar volumes of Fe and FeO are
274	plotted in Figure 2, and the corresponding ΔV_{IW} is plotted in Figure 4. Although MAP
275	experiments can be performed at a predetermined temperature, controlled by feedback
276	from the thermocouple, laser-heated DAC experiments do not so easily permit a tightly
277	specified temperature, and the temperature values are usually determined after the fact.
278	For this reason, the data in the figures are coded by temperature range, rather than plotted
279	as sets of isothermal data.

In Table S3, all of the Ni data refer to the fcc structure, and all of the NiO datarefer to the B1 structure. No other phases were observed. The molar volumes of Ni and

- NiO at high pressure and temperature are plotted in Figure 3, and the ΔV_{NNO} values are
- 283 plotted in Figure 4.

4. Discussion

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288 4.1. Equations of state and ΔV_{ox-met} at high pressures and temperatures

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290 In many geophysical applications, the difference in molar volume (or density) 291 between phases is more important than the absolute volumes (or densities) of those 292 phases. The application that we intend for the present data, calculating the 293 thermodynamics of chemical equilibria at high pressure, is one example. In these cases, 294 there are significant advantages to measuring the two phases simultaneously, under 295 identical P,T conditions, rather than comparing two independently determined equations 296 of state to one another. Equation of state studies can suffer from systematic biases resulting from their experimental procedures. For example, pressure standards are not all 297 298 perfectly consistent with one another. Although there is ongoing work in improving this 299 situation by comparing pressure standards to one another (Fei et al., 2007; Dorogokupets 300 and Oganov, 2007; Dewaele et al., 2008), there is already a voluminous literature in 301 which various, inconsistent pressure scales were used. When it is critical to compare the 302 volumes of two phases directly, a better strategy is to measure them simultaneously to 303 avoid problems related to inconsistency in pressure standards. Furthermore, holding the 304 two phases together under high P,T conditions allows them to reach chemical equilibrium 305 with one another. This is a very important advantage when there is a new phase, or new 306 stoichiometry, that exists in the system only at high P and T, and not under ambient 307 conditions. This is the case in the Fe-FeO system. At 1 bar the stoichiometric Fe_{1.00}O 308 phase is not stable, but at high-P,T conditions non-stoichiometric wüstite can react with 309 metallic Fe to form Fe_{1.00}O (Stølen and Grønvold, 1996); this fact was exploited in the 310 present study. For all of these reasons, we chose to measure $\Delta V_{\text{ox-met}}$ in the Fe-FeO and Ni-311 NiO systems by simultaneous measurement of the molar volumes of metal and coexisting 312 oxide at high pressures and temperatures. This strategy improves the precision to which

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313 the ΔV values are determined, thereby improving the calculation of oxygen fugacity 314 buffers at high pressure.

315 High pressure, high temperature equations of state were derived for each phase by316 fits to the combined MAP and DAC data. A Mie-Grüneisen equation of state was used,

317 (5) $P = P_{295}(V) + (\gamma/V) [E(\theta_D, T) - E_{295}(\theta_D, 295)]$

318 with the 295 K isotherm (P_{295}) described by a Birch-Murnaghan equation and the thermal 319 pressure term based on a Debye model of vibrational energy (E), with Grüneisen 320 parameter $\gamma = \gamma_0 (V/V_0)^q$ and Debye temperature $\theta_D = \theta_0 (V/V_0)^{\gamma}$. Although this formalism 321 does not explicitly include parameters for anharmonic or electronic contributions, it is 322 identical to that used to describe the NaCl-B2, Pt, Au, and Ne equations of state by Fei et 323 al. (2007). Parameters used in the least-squares fits to the equation of state data are presented in Table 1. We do not offer an alternative set of equation of state parameters for 324 325 hcp-Fe, because no fit to our data was superior to the Dewaele et al. (2006) equation, so 326 we used it in our analysis instead. (The agreement between our data and the Dewaele et 327 al. (2006) equation for hcp-Fe is further evidence that the NaCl pressure medium can act 328 as an effective pressure standard, as described above, during high temperature laser 329 heating experiments when stress gradients have been relaxed.)

330 By combining data from the two different experimental methods (MAP and 331 DAC), we were able to investigate a more complete range of pressures and temperatures 332 than either method can cover alone. In principle this approach provides a more robust 333 equation of state, but one potential concern is that two different pressure standards were 334 used among the measurements (NaCl-B1 for low pressures; NaCl-B2 for high pressures). 335 Residuals from the fitted equations of state in Table 1 do not reveal systematic biases 336 between the two methods or between the two pressure calibrations. However, this may 337 simply be a consequence of there being little overlap in P,T conditions covered by the 338 two methods, and larger uncertainties related to the thermal gradient across the NaCl 339 standard in the laser heated DAC experiments. Overlapping measurements at low

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340	pressure and high temperature were precluded by melting of the NaCl standard, so direct
341	comparisons cannot easily be made between the complementary but separate data sets.
342	The present results therefore rely on the accuracy of the widely used equation of state of
343	NaCl-B1 (Decker, 1971) and the fact that the NaCl-B2 equation of state has been cross-
344	calibrated against multiple other P-V-T standards (Fei et al., 2007).
345	Volume differences (Figure 4) between NiO and Ni, ΔV_{NNO} , and between FeO and
346	Fe, ΔV_{IW} , are also included in Tables S2 and S3. There is no functional form that one
347	should expect the ΔV -P-T data to follow, so the ΔV data were not fit to an equation.
348	Instead, in the calculations below the ΔV values were determined numerically from the
349	fitted equations of state given in Table 1; the volumes at each pressure and temperature
350	were determined iteratively to a precision of $< 10^{-4}$ GPa in pressure.
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352	4.2. Calculation of high pressure buffers
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354	In this section we use the analyses of ΔV - <i>P</i> - <i>T</i> data in Section 4.1 to calculate the
355	NNO and IW (strictly, Fe-FeO) oxygen fugacity buffer curves at high pressures. The
356	calculations proceed by integration of Eqn. (3), with $x=1$ for both FeO and NiO:
357	(6) $\log fO_2 = \log fO_2(1 \text{ bar}) + (0.8686/\text{R}T) \int \Delta V dP$
358	where the conversion from ln to \log_{10} was made. The 1 bar fO_2 buffers were calculated
359	using the thermodynamic data in Chase (1998) for stoichiometric FeO and Knacke et al.
360	(1991) for NiO. Only ΔG data below the melting points were used, but extrapolations of
361	these data to higher temperatures was made to facilitate analysis of high- P,T data. High
362	pressure fO_2 buffer curves were calculated along a set of isotherms from 1000 K to 2600
363	K, in 100 K intervals. Integration of $\Delta V dP$ for each metal-oxide system utilized the ΔV
364	values calculated from the equations of state above. For the IW system, integration
365	proceeded using the fcc-Fe data up to the fcc-hcp transition pressure (Shen et al., 1998) at

each temperature; above this transition pressure the ΔV_{IW} data for hcp-Fe were used in the integration.

368 The IW buffer at 1 bar and at high pressures is shown in Figure 5a. Tabulated 369 values at smaller pressure increments are presented in Table S4 in the Supplementary 370 Material. There are two primary effects of pressure on the IW fO_2 curve. The first is that 371 the absolute fO_2 values increase with pressure at each temperature. The second effect is 372 that the slope $\partial(\ln fO_2) / \partial T_{\rm P}$ decreases with pressure, eventually becoming a slope of 373 approximately zero at 60 GPa, and negative at higher pressures. At pressures higher than 374 60 GPa, the slope of the oxygen fugacity curve with T is negative, so at a fixed fO_2 , 375 increasing temperature drives Fe toward oxidation. This is the opposite of the behavior 376 familiar at 1 bar or other low-pressure conditions, and is not specific to the Fe-FeO 377 buffer. Any oxygen fugacity buffer will eventually obtain a negative $\partial (\ln fO_2) / \partial T_{\rm P}$ slope 378 at high pressure, because the pressure derivative $\partial(\ln fO_2) / \partial P|_T$ is greater at low 379 temperatures than it is at high temperatures, following Equation (3).

380 The analogous calculation for the NNO buffer curves at 1 bar and at high 381 pressures is illustrated in Figure 5b (calculated values in Table S5 of Supplementary 382 Material). These curves are always higher than the IW buffer curves at the same pressure, 383 reflecting the higher siderophility of Ni relative to Fe. However, the pressure effect on the 384 NNO buffer is not as great as that for the IW buffer, because ΔV_{NNO} is smaller than ΔV_{IW} . 385 Consequently, the difference between the NNO buffer and the IW buffer decreases with 386 pressure. For example, at 1500 K this difference is 4.78 log fO_2 units at 1 bar but only 387 2.38 $\log_{f}O_{2}$ units at 60 GPa. One way to view this is that Ni becomes less siderophile 388 with increasing pressure.

To illustrate more explicitly how the difference between the buffer curves (NNO-IW) varies with pressure, these values are plotted in Figure 5c. This figure allows one to quickly evaluate the difference between the buffers at any *P*,*T* condition within the range covered by this study. More precise values can be determined from Tables S4 and S5 in

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393 the Supplementary Material, where numerical log fO_2 values for the IW and NNO oxygen 394 fugacity buffers are listed, and coefficients to a polynomial fit to the log fO_2 values are 395 also provided. Misfits to the equations of state produce r.m.s. values on ΔV of 396 approximately 0.03 cm³/mol for both buffers; this contributes uncertainty to the 397 calculated buffers that is proportional to P/T, reaching ±0.2 log units at 100 GPa and 398 1500 K.

Contrary to the low pressure circumstances, the difference between the two
buffers has a negative slope above ~50 GPa (Figure 5c). This implies that at high
pressures Ni becomes more siderophile with increasing temperature; Kegler et al. (2008)
noted a similar effect in their data regression, but at somewhat lower pressure, ~30 GPa.

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404	4.3 Applications
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406 As petrological and geochemical studies extend deeper into the Earth, it is 407 necessary to have a thermodynamic framework in place in which to interpret the data. 408 The present study is a step in this necessary direction, by extending two commonly used 409 buffers to great depths in the Earth and illustrating the pressure-induced changes in the 410 difference between them. One might consider how the Fe-FeO and NNO buffers relate to 411 one another along the pressure-temperature path in the Earth's deep mantle. We show this 412 comparison in Figure 6, in which the values of these two buffers are shown along a 413 representative geotherm, in this case the Brown and Shankland (1981) model. At 1 bar 414 and 1400 K, the difference between the NNO and Fe-FeO buffers is 5.0 log units. By 670 415 km (23.8 GPa by PREM (Dziewonski and Anderson, 1981) and 1873 K by Brown and 416 Shankland (1981)), this difference has dropped to 3.4 log units, and at 2000 km depth (86.9 GPa, 2256 K) the difference is only 2.1 log units. This relative change in the metal-417 418 oxide buffers should manifest itself in changing chemical behavior of Ni. The oxygen 419 fugacity of the mantle is largely reflected in the redox state of Fe, and there is a body of

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420 evidence that much of the mantle is saturated in Fe-rich metal (Frost and McCammon, 421 2008), so the mantle fO_2 should lie just below the Fe-FeO buffer shown in Figure 6. The 422 exchange of Fe and Ni between phases will vary with depth according to the variation in 423 differences in buffers shown in the figure. One expects on this basis that Ni will be less 424 strongly siderophile at depth, relative to Fe.

425 More generally, the pressure dependence on differences in fO_2 buffers can play a 426 role in understanding, from a thermodynamic perspective, why chemical partitioning 427 behavior varies the way it does with pressure. For example, as pressure and temperature 428 increase, the NNO and IW buffer curves converge (Figure 5c); in essence, Ni becomes 429 less siderophile. Holding other factors (namely activity coefficients) equal, one would 430 then expect that with increasing pressure, the Ni-Fe exchange coefficient between metal 431 and silicate or oxide would decrease. This is in fact observed; partitioning studies between liquid silicate and metal show that $K_{met/sil}^{Ni-Fe}$ decreases with increasing pressure 432 433 (Thibault and Walter, 1995; Li and Agee, 1996; 2001; Bouhifd and Jephcoat, 2003; 434 Corgne et al., 2008). There is an extensive literature from these experimental studies, 435 principally with the goal of understanding chemical exchange and equilibration between 436 the silicate mantle and the segregating core during early Earth differentiation. 437 Parameterizations in P, T, fO_2 , and nbo/t have been crucial to comprehensive 438 understanding of metal/silicate partitioning (Righter et al., 2003). Evolution of these 439 parameterizations, using more robust thermodynamic treatment of the oxygen fugacity 440 states in the experiments, is a natural way to augment the existing data to improve its 441 accuracy and power of prediction, and also to better guide future experimentation.

442 Metal silicate partition coefficients ($D = X^{\text{met}}/X^{\text{sil}}$) are commonly parameterized 443 with linear dependence on temperature, pressure, oxygen fugacity, silicate polymerization 444 (*nbo/t*), and/or sulfur (X_{s}) and carbon (X_{c}) content of the metallic melt (e.g., Righter, 445 2003):

446 (7) $\log D = a + bT + c(P/T) + d\log fO_2 + e(nbo/t) + f\log(1-X_s) + g\log(1-X_c)$

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This method has been shown to be effective at describing experimental data over the
range of their measurement conditions (Righter, 2003). However, extrapolations must be
treated with caution because of the assumed linearity. Here, we recast this equation to
permit nonlinear dependence on pressure:

451 (8)
$$\log D = \Delta G^{\text{MMO}} / (\text{RTln10}) - \log (\gamma_{\text{M}} / \gamma_{\text{MOx}}) - \frac{x}{2} \log fO_2$$

where the most of the pressure dependence is in the ΔG^{MMO} term through equations (3) and (6), although there may also be pressure dependence to the activity coefficients, γ (i.e., nonzero mixing volumes). The fO_2 dependence of metal-silicate partitioning is strong, and it is useful to eliminate it by considering, instead of the partition coefficient, an exchange coefficient, K_{D} . For M-Fe exchange:

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(9)
$$K_{\rm D} = D({\rm M}) / D({\rm Fe})^{\rm x} = (X_{\rm M}^{\rm met}/X_{\rm MOx}^{\rm sil}) / (X_{\rm Fe}^{\rm met}/X_{\rm FeO}^{\rm sil})^{\rm x}$$

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$$\log K_{\rm D} = \frac{x}{2} \left(\log f O_2^{\rm MMO} - \log f O_2^{\rm IW}\right) + \log \left(\gamma_{\rm MOx}^{\rm sil} / \gamma_{\rm M}^{\rm met}\right) / \left(\gamma_{\rm FeO}^{\rm sil} / \gamma_{\rm Fe}^{\rm met}\right)^{\rm x}$$

459 from equations (2) and (8).

(10)

460 We can use equation (10), combined with the high pressure values of $\log fO_2^{NNO}$ -461 $\log fO_2^{IW}$ calculated in the previous section, to predict the pressure dependence of Ni-Fe 462 exchange between metal and silicate. In Figure 7 the ratio of activity coefficients is chosen to satisfy the low pressure experimental data for $K_{met/sil}$ ^{Ni-Fe} between iron-rich 463 464 metallic melt and mafic silicate melt (Li and Agee, 1996; Ito et al., 1998), and equation 465 (10) is applied with our results on the fO_2 buffers of Ni-NiO and Fe-FeO to predict the pressure dependence of $K_{met/sil}^{Ni-Fe}$. We use the Li and Agee (1996) and Ito et al. (1998) 466 467 studies to make this comparison, because in each of these studies the metal and silicate 468 compositions remained nearly constant (although they differ between the two data sets), 469 and both reached fairly high pressure. Two assumptions are made in this calculation. 470 First, it is assumed that the activity coefficients (or at least the ratio of activity 471 coefficients) are constant with pressure. Second, the calculation assumes that the free energy differences between solid and liquid (ΔG_{liquid} ^{MMO}- ΔG_{solid} ^{MMO}) are equal for the Ni-472 473 NiO system and the Fe-FeO system. This assumption is necessary because, although our

high pressure buffer curves are calculated for the solid metal-oxide systems, experimental
studies of metal-silicate partitioning are generally applied to liquid systems, because their
principal application is to elemental partitioning in the conditions of a magma ocean
during differentiation of the early Earth. More rigorously, including the solid-to-liquid
terms in deriving equation (10) produces:

(11)

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 $\log K_{\rm D} = {}^{\rm x}/_2 \left(\log f O_2^{\rm MMO} - \log f O_2^{\rm IW}\right) + \log \left(\gamma_{\rm MOx} {}^{\rm sil}/\gamma_{\rm M} {}^{\rm met}\right) / \left(\gamma_{\rm Fe0} {}^{\rm sil}/\gamma_{\rm Fe} {}^{\rm met}\right)^{\rm x} + \left[\left(\Delta G_{liquid} {}^{\rm MMO} - \Delta G_{solid} {}^{\rm MMO}\right) - {\rm x} \left(\Delta G_{liquid} {}^{\rm IW} - \Delta G_{solid} {}^{\rm IW}\right)\right] / \left({\rm R}T\ln 10\right)$

481 Equation (10) is otherwise exact, and deviations away from the prediction of this482 equation must reflect violations of these two assumptions.

483 As shown in the figure, equation (10) accurately describes the pressure dependence of $K_D^{\text{Ni-Fe}}$ up to approximately 10-15 GPa, when the activity coefficient ratio 484 is chosen to match the low pressure $K_D^{\text{Ni-Fe}}$ value. However, at higher pressures the 485 486 observed metal-silicate partitioning decreases more rapidly than predicted by equation 487 (10). One interpretation is that the assumption of constant activity coefficient ratios is 488 violated at high pressure, and the mixing volume of one or more species becomes 489 nonzero at high pressure. This could be related to coordination changes of these transition 490 elements, analogous to those reported in albite melts by Keppler and Rubie (1993), as 491 well as more general structural changes in the silicate melt, that are known to occur in 492 this pressure range (Williams and Jeanloz, 1988; Stebbins et al., 1995; Stixrude and 493 Karki, 2005). Kegler et al. (2008) reported a similar change in the pressure dependence 494 of $K_D^{\text{Ni-Fe}}$ that they attributed to coordination changes in the silicate melt, although their observed change in $K_D^{\text{Ni-Fe}}$ behavior occurred at lower pressure (~5 GPa) than seen in 495 496 Figure 7. Another interpretation of the departure of the experimental data from the 497 equation (10) curve is that the solid-to-liquid correction is significant, and our assumption that the free energy difference ($\Delta G_{liauid}^{MMO} - \Delta G_{solid}^{MMO}$) is everywhere equal 498 499 between the Ni-NiO system and the Fe-FeO system is invalid. In this case the pressure dependence of metal-silicate partitioning will require knowledge of the volumes of the 500

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melt components, and their pressure dependence. The experimental data on melt components are very limited in pressure, and these have been shown to predict the pressure dependence of K_D only qualitatively (Courtial et al., 1999).

504 To illustrate the possible effect of this reformulation of the metal/silicate 505 partitioning data, we postulate the emergence of a nonzero mixing volume for the Ni-Fe 506 exchange reaction above 10 GPa, pursuant to the discussion above. As shown in Figure 7, 507 a mixing volume of -1.5 cm³/mol satisfies the difference between our predicted highpressure behavior for $K_D^{\text{Ni-Fe}}$ and the results of Li and Agee (1996). (The suddenness of 508 509 the mixing volume change shown in Figure 7 is a simplification.) On the basis of linear 510 extrapolations to their experimental data, Li and Agee (1996) calculated that the Ni and 511 Co abundances in the upper mantle can be explained by partitioning during Earth's core-512 mantle equilibration in a magma ocean at pressures between 28 and 42 GPa. Our reparameterization of the $K_D^{\text{Ni-Fe}}$ data, assuming $\Delta V_{\text{mixing}} = -1.5 \text{ cm}^3/\text{mol}$ (and leaving the 513 514 Co-Fe exchange parameterization unchanged from Li and Agee (1996)), produces the 515 same degree of partitioning at a lower pressure range, between 24 and 36 GPa. Hence, this change to the parameterization of $K_D^{\text{Ni-Fe}}$ can impact the inferred pressure of core-516 517 mantle equilibration.

The linear pressure dependence of log $K_D^{\text{Ni-Fe}}$ that is fitted empirically to high 518 519 pressure metal-silicate partitioning data (e.g., Li and Agee, 1996; Righter et al., 1997; 520 Righter, 2003; Corgne et al., 2008) data masks two underlying thermodynamic effects, 521 shown in equations (10) and (11). First, the pressure dependence can be understood 522 simply in terms of the volume differences between the Ni-NiO and Fe-FeO buffers, that 523 are components dissolved into the metal and silicate melts. Second, the ratios of activity 524 coefficients relevant to this mixing obtain pressure dependences (nonzero mixing 525 volumes) at pressures above approximately 10-15 GPa (Figure 7), likely in response to 526 the changing structural coordinations in the silicate melt at this pressure. Over the 527 pressure range obtained by the multi-anvil press data, the pressure dependence of K_D

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528 frequently is well described by a linear term, allowing accurate interpolation and 529 description of the data over this pressure range. However, it is understood that the 530 functional form of the thermodynamic expressions driving this pressure dependence may 531 not be linear, and as illustrated by the example above, with extrapolation to higher 532 pressures and temperatures a linear parameterization will be prone to increasing 533 inaccuracy. It follows that a more thorough analysis of numerous metal-oxide buffers, 534 using their (solid and/or liquid) equations of state at high pressures, offers the prospect of 535 yielding greater resolution of volume vs. structural effects on metal-silicate partitioning 536 of moderately siderophile elements, that will provide more reliable extrapolations to deep 537 Earth conditions to better interpret observed mantle chemistry in terms of the chemical 538 effects of core-mantle segregation.

539

540 5. Summary

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542 The effect of pressure on oxygen fugacity buffers is calculable to high precision, 543 if a full high pressure, high temperature equation of state is applied for the coexisting 544 species instead of assuming a fixed ΔV . Systematic biases between pressure calibrations 545 of equation of state measurements can be minimized by measuring the two (metal and 546 oxide) components together. Furthermore, this approach ensures that the metal and oxide 547 chemically equilibrate with one another, for example driving the iron oxide component to Fe_{1.00}O stoichiometry in the experiments. This method was applied here to the Fe-FeO 548 549 and Ni-NiO systems, using two complementary experimental methods, a multi-anvil 550 press and diamond anvil cells, for maximum *P*-*T* coverage.

551 The Ni-NiO and Fe-FeO oxygen fugacity buffers both increase with pressure, but 552 at different rates, such that the difference between them diminishes with pressure. This change in relative $\log fO_2$ units is important to consider when comparing results from 553 554 high-pressure experimental runs referenced to the Fe-FeO vs. the Ni-NiO buffers. Along 555 the P-T path of a nominal mantle geotherm, the difference between the Ni-NiO and Fe-556 FeO buffers is reduced by nearly three \log_{fO_2} units over 2000 km depth in the Earth. 557 This diminishing siderophile nature of Ni is consistent with experimental studies of 558 metal-silicate partitioning of Ni and Fe. The formalism used here allows us to better interpret these data, emphasizing that the pressure effect on $K_D^{\text{Ni-Fe}}$ has two components, 559 560 an intrinsic volumetric effect and a possible mixing volume term above 10 to 15 GPa 561 related to structural changes in the silicate melt. With further study covering a variety of 562 moderately siderophile elements, this view of high pressure geochemical behavior should 563 permit improved extrapolations to the inferred conditions of metal-silicate equilibration 564 during Earth's core formation.

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568

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740	

741 Figure Captions

743	Figure 1. Sample geometry and temperature distribution in the laser heated diamond
744	anvil cell experiments. The sample, a mixture of metal+oxide powders, was embedded in
745	a NaCl pressure medium that also acted as a thermal insulator and pressure standard,
746	using the equation of state for the B1 (Decker, 1971) or B2 (Fei et al., 2007) phases. The
747	temperatures were measured at the intersection of the x-ray beam with the two surfaces
748	of the opaque sample. Temperature distributions internal to the sample were calculated
749	by Campbell et al. (2007). The temperature profile across the NaCl insulator is
750	approximated as linear, with a mean temperature between that measured at the sample
751	surface (T_{meas}) and the diamond anvil, whose surface temperature is between T_{meas} and 295
752	К.
753	
754	Figure 2. Equation of state data for Fe and FeO. Data below 15 GPa were obtained by
755	MAP; higher pressure data were obtained by DAC (this study and from Seagle et al.
756	(2008)). Squares: fcc-Fe; circles: hcp-Fe; triangles: FeO. Only the B1 phase of FeO was
757	observed in coexistence with Fe at high pressure and temperature. The data were
758	obtained only at P,T conditions sufficiently high to ensure stoichiometric Fe _{1.000} O (Stølen
759	and Grønvold, 1996). Data are color coded to indicate temperature. Shown for
760	comparison are the Dewaele et al. (2006) equation of state for hcp-Fe and equations of
761	state from Table 1 at various temperatures. Each colored curve represents the midpoint of
762	the temperature range indicated.
763	
764	Figure 3. Equation of state data for Ni and NiO. Data below 15 GPa were obtained by
765	MAP; higher pressure data were obtained by DAC. Circles: Ni; triangles: NiO. Data are
766	color coded to indicate temperature. A Mie-Grüneisen equation of state is fit to the data at

different temperatures as shown. Each colored curve represents the midpoint of thetemperature range indicated.

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Figure 4. Volume differences between coexisting oxide and metal at high pressures and
temperatures, from the data in Figures 2 and 3. Diamonds: FeO-fcc Fe; circles: FeO-hcp
Fe; squares: NiO-Ni.

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774 Figure 5. (a) Fe-FeO and (b) Ni-NiO oxygen fugacity buffers, and (c) the difference 775 between them, at various pressures. The 1 bar buffer curves were calculated from Chase 776 (1998) and Knacke et al. (1991), and high pressure curves were calculated from Equation 777 (6) using fits to the data like those in Figures 2 and 3. With increasing pressure and 778 temperature, the difference between the Ni-NiO and Fe-FeO buffers decrease, indicating 779 decreasing siderophility of Ni. Uncertainties are indicated in (c) by vertical bars. 780 781 Figure 6. Fe-FeO and Ni-NiO oxygen fugacity buffers along a representative geotherm 782 through the Earth's mantle (Brown and Shankland, 1981; Dziewonski and Anderson, 783 1981). At 2000 km depth, the pressure and temperature are 86.9 GPa and 2256 K. The 784 difference between the two buffers decreases from 5.0 log units at 1 bar, 1400 K to 2.1 785 log units at 2000 km depth. 786 787 Figure 7. Exchange coefficient (K_D) for Ni and Fe between metallic melt and peridotitic

silicate at high pressure. Shaded circles: Li and Agee (1996). Open squares: Ito et al.

(1998). Solid curve: calculated pressure dependence based on equation (10) and

experimental equation of state results of this study, assuming that the activity coefficient

term in eqn. (10) is constant with pressure. The curve predicts the pressure dependence at

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low pressures, but above 10 GPa the curve deviates from the data, suggesting nonideal

- mixing related to changes in the silicate melt structure. Dashed curve: shows the effect of
- a mixing volume of -1.5 cm³/mol applied above 10 GPa.

Table 1. Equation of state (Birch-Murnaghan)) parameters.
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	Fe-fcc	FeO-B1	Ni	NiO
V_0 , cm ³ /mol	7.076 ^a	12.256 ^b	6.587 ^a	10.973 ^a
K, GPa	133 ± 3	146.9 ± 1.3	179 ± 3	190 ± 3
Κ'	5 ^c	4^{d}	4.3 ± 0.2	5.4 ± 0.2
$\Theta_{\rm D}, {\rm K}$	470 ^e	380 °	415 ^j	480 ^r
γο	1.95 ± 0.04	1.42 ± 0.04	2.50 ± 0.06	1.80 ± 0.04
q	1.6 ± 0.6	1.3 ± 0.3	1	1

Entries in italics held fixed in the fit: ^aJCPDS card files. ^bMcCammon, 1984. ^cFunamori et al., 1996. ^dFei, 1996. ^cChase,1988. ^tKnacke et al., 1991.











Figure 5





Supplementary Material

Supplementary Figure S1. Representative X-ray diffraction data obtained while laser heating a Ni+NiO sample in a diamond anvil cell. The graph shows the diffraction pattern obtained by azimuthal integration of the 2-D diffraction image. The white region in the center is caused by a beam stop blocking the primary X-ray beam. Inset: X-ray diffraction image. The spottiness of the diffraction rings is a consequence of recrystallization upon heating.

Supplementary Table S2. Pressure-volume-temperature data from X-ray diffraction experiments on Fe+FeO.

Supplementary Table S3. Pressure-volume-temperature data from X-ray diffraction experiments on Ni+NiO.

Supplementary Table S4: Fe-FeO oxygen fugacity buffer from 1000 to 2600 K and 0 to 100 GPa.

Supplementary Table S5: Ni-NiO oxygen fugacity buffer from 1000 to 2600 K and 0 to 100 GPa.

